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LASER WITH WIDE OPERATING TEMPERATURE RANGE

DESCRIPTION

Technical field

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~~This invention relates to the field of quantic well lasers comprising a reflection means external to the laser cavity.~~

5 Technological background

out a2
~~Patent US-A-5 715 263 issued to SDL describes an example of a laser shown in figure 2 of this patent comprising a quantic well laser 26 with an output mirror 27 outputting into an optical fiber 32. This type of laser is used in telecommunications to pump an amplifier outputting into a transmission line. According to the invention described in the SDL patent, the fiber 32 comprises a fiber Bragg network 34 with the function of reflecting part of the light emitted by the laser 26 back to the laser 26. This patent (column 2, lines 37-45) describes how the optical spectrum of the emitting laser diode is affected if the center of the reflection band of the fiber Bragg network is in the laser gain band. The exact effect depends on parameters such as the value of the reflection coefficient and band width of the fiber Bragg network, the central wavelength of the network with respect to the laser, the value of the optical distance between the laser and the network, and the value of the current injected into the laser. In the SDL patent, the~~

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central wavelength of the Bragg network is contained within a 10 nm band around the laser wavelength and the value of the reflection coefficient of the network 34 is similar to the value of the output face 27 from laser 26. In the preferred embodiment, the width of the band reflected by the network 34 and its reflection coefficient are such that the return into the laser cavity due to the output face is greater than the return due to the network 34. Consequently, the network 34 acts like a disturbance to the emission spectrum of laser diode 26, which has the effect of widening the emission band and thus making the diode less sensitive to disturbances caused by temperature changes or injected currents.

In order to obtain the required effect, in the preferred embodiment the network 34 has a reflection peak that is located 1 or 2 nm from the wavelength of the diode, a reflection coefficient of 3% which, taking account of coupling between the network and the diode, produces a return coefficient to the diode equal to 1.08%.

Patent US A 5 563 732 issued to AT&T Corp. also describes a pumping laser 13 for an amplifier laser 12 also used to make optical transmissions. This laser 12 is stabilized to prevent fluctuations in the emitted wavelengths caused by parasite reflections from the amplifier laser 12 by means of a fiber network 14. The inventors have found that the pumping laser 13 is stable if the reflection coefficient from the network 14 is between 5 and 43 dB.

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~~Experiments carried out by the applicant have~~
 shown that the use of lasers stabilized using a fiber
 network can have a good influence on the operating
 stability of the laser and particularly on the
 5 stability of the emitted wavelength, but only within
 certain limits. In particular, the use of lasers
 stabilized as described in each of the two patents
 mentioned above cannot produce a laser capable of
 operating within a temperature range varying from -20°C
 10 to +70°C as currently required by most users.
~~Therefore there is a need for such a laser.~~

Brief description of the invention

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~~The invention relates to a quantie well laser like~~
 15 the lasers described in the two documents mentioned
 above, but which is capable of operating without any
 particular precautions within a temperature range
 between two limiting temperatures defining a range of
 about 100°, and particularly within the temperature
 20 range from -20°C and +70°C. However, it should be
 understood that operating between -20°C and +70°C is
 not the same thing as widening the operating band in
 order to give a band with an output wavelength
 independent of reasonable fluctuations in the operating
 25 temperature, for example within a temperature range
 fluctuating by 5 to 6° about a nominal operating
 temperature.

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~~As in prior art, the invention uses a quantie well
 laser with a laser cavity formed by a laser medium~~

~~between a reflection face and an output face with a reflection coefficient,~~

- means of coupling the laser output to an optical fiber,
- 5 - the optical fiber with a fiber network returning a fraction of the light received from the laser through the fiber, to the laser cavity through ~~coupling means.~~

al ar
~~However, the invention is different from prior art~~
 10 in one important respect. The inventors have observed that, at a given temperature, the gain curve for the cavity as a function of the wavelength, has a positive slope in the direction of increasing wavelengths, is maximum at a wavelength λ_{max} , and then has a negative
 15 slope. The slope coefficient of the positive slope is much smaller than the slope coefficient after the maximum. By observing the manner in which the gain curve deforms as a function of the temperature, they found that, for example for a laser operating at 980 nm
 20 at 25°C, the maximum shifted between 966 at -20°C and about 995 nm at 70°C. The displacement is approximately linear with a coefficient of about 0.3 nm per degree. For the system to operate over a wide temperature range, it is necessary that the condition
 25 under which the cavity gain is equal to cavity losses is satisfied for the wavelength of the fiber Bragg network over the entire temperature range, despite deformations to the cavity gain curve as a function of the wavelength caused by temperature variations. The
 30 ~~inventors found that this condition can be satisfied if~~

~~the value of the reflection wavelength of the fiber~~
 network at the median temperature is at least 10 nm
 less than the value of the wavelength λ_{\max} for which the
 cavity gain is maximum. In practice, the amount to be
 5 provided should be 15 plus or minus 5 nm. The fact of
 using a value of the wavelength equal to about 15 nm
 before this maximum means that the threshold condition
 at which the gain is equal to losses can be satisfied
 over a wide temperature range, at the network
 10 ~~wavelength.~~

~~In summary, the invention relates to an optical~~
 109 device comprising:

- 15 - a quantic well laser with a laser cavity formed
 by a laser medium between a reflection face and
 an output face reflecting part of the light
 energy to the cavity, the curve representing the
 gain of the cavity as a function of the
 wavelength having a positive slope for
 increasing wavelengths, a maximum for a
 20 wavelength λ_{\max} and then a negative slope,
- means of coupling the laser output to an optical
 fiber, the optical fiber having a fiber network
 defining a coefficient of a reflection peak for
 a wavelength λ and reflecting a fraction of the
 25 light received from the laser through the fiber,
 to the laser cavity through coupling means,
- device characterized in that the value of the
 wavelength λ defining the reflection peak of the
 fiber Bragg network is less than the value of
 30 ~~the wavelength λ_{\max} by at least 10 nanometers.~~

at a10
~~Preferably, the energy received by the laser~~
~~cavity returning from the fiber network is greater than~~
~~the energy received in return through the laser output~~
~~face.~~

at a11
 5 ~~This functional characterization may be clarified~~
 by a structural characterization defining a ratio
 relating the coefficients of the laser output face and
 the network reflection coefficient. The product of the
 reflection coefficient for the fiber network and the
 10 square of the loss coefficient due to coupling between
 the fiber and the laser must be greater than the
 reflection coefficient at the cavity output face. In
 this way, the energy received in return from the fiber
 network can no longer be considered as being a
 15 disturbance widening the output optical spectrum. The
 value of the wavelength reflected by the network
 determines the value of the laser output wavelength.
 In a known manner, the value of the wavelength λ
 reflected by the fiber network varies with temperature
 20 much less than the cavity. The result is that with
 this configuration, the optical system formed by the
 laser, the fiber and the coupling means is capable of
 operating while remaining less dependent on local
 temperature variations. In one embodiment of the
 25 invention, the value of the network reflection
 coefficient is more than ten times greater than the
~~reflection coefficient from the laser output face.~~

Brief description of the drawings

An example embodiment of the invention will now be commented upon and explained using the attached drawings in which:

- 5 - figure 1 is a diagram representing an embodiment of the invention.
- Figure 2 is a set of three pairs of curves, each pair representing the gain and losses of the laser cavity. The pair of curves A represents the gain and losses of the laser cavity at 25°C, and the pair of curves B and C represent the gain and losses of the laser cavity at 70°C and -25°C respectively.

Description and comments for one embodiment

15 ~~Figure 1 diagrammatically shows a laser cavity 1~~
~~laid out in a manner known per se such that the~~
~~direction of the emitted laser beam is controlled by~~
~~focusing optical means 2 into an optical fiber 5~~
~~comprising a fiber network 6 in a known manner. The~~
20 ~~laser 1 may be composed of a laser diode comprising an~~
~~epitaxied quantic well structure, in a known manner as~~
~~described for example in the patent mentioned above US-~~
~~A-5 715 263, or an InGaAs semiconducting medium between~~
~~a reflecting mirror 8 and an output face 9 with a~~
25 ~~reflection coefficient that is very low compared with~~
~~the reflection coefficient of the mirror 8. The laser~~
~~cavity is formed between mirrors 8 and 9.~~

The optical focusing means are composed of a first collimation lens 3 followed by a focusing lens 4 that

focuses light towards the center of the fiber 5, in a known manner.

5 The characteristic features of the invention will
 now be explained and commented upon in relation to the
 curves in figure 2. Part A in the figure shows the
 curve 10 representing the gain of the laser cavity as a
 function of the wavelength, and curve 11 represents the
 losses of the same cavity as a function of the
 wavelength. The laser can only operate if losses are
 10 lower than the gain. In the case of the device shown
 in figure 1, the value of the reflection coefficients
 from the cavity output face 9 and the network 6 are
 such that this only occurs for the wavelength λ that is
 the reflection wavelength of the network 6. This is
 15 due to the fact that the quantity of light reflected by
 the network is greater than the quantity of light
 reflected by the output face 9. In the case shown in
 figure 1, the value of the reflection coefficient of
 the output face 9 is typically 0.1% whereas the value
 20 of the reflection coefficient of the network 6 is
 typically of the order of 1%, and in any case remains
 less than or equal to 5%. With this method of choosing
 the relative values of reflection coefficients, the
 emission frequency of the laser within the range
 25 authorized by the medium is determined by the
 reflection wavelength of the network. As described
 above, the result is very good operating stability. We
 will consider deformations of curves 10 and 11 when the
 temperature varies. The curves in part A represent
 30 operation at 25°C. The same curves 10 and 11 were

~~shown in parts B and C in figure 2 for temperature~~
 values equal to $+70^{\circ}\text{C}$ and -20°C respectively. The
 first noticeable fact is that there is practically no
 deformation in curve 11 representing losses, and all
 5 that happens is that the value of λ is slightly
 shifted. The gains curve 10 shows a small positive
 slope for small values of the wavelength, and is then
 equal to a maximum, and then has a steep negative
 slope. This is satisfied for the three temperatures
 10 shown. It can be seen that for increasing
 temperatures, the maximum shifts by a relatively large
 amount towards increasing values of the wavelength, and
 that the maximum increases with temperature such that
 the length of the line with a positive slope increases.
 15 The inventors chose a value of the reflection
 wavelength λ of the network 6 at the required median
 operating temperature, equal to about 13 nm less than
 the value of the wavelength at the maximum on the gain
 curve 10 at the same temperature. In this case, the
 20 required operating range is -20°C to $+70^{\circ}\text{C}$. Therefore,
 the median temperature of this range is 25°C . With
 this choice as shown in part B, there is still a
 possible and stable operating point for the value of
 the reflection wavelength λ of the network 6 at the
 25 maximum temperature in the range. Similarly at -20°C ,
 the minimum temperature in the range and shown in part
 C in figure 2, there is still an operating point at the
 maximum on curve 10 located at a value of the
~~wavelength close to the reflection wavelength λ of the~~

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~~network 6 at this temperature. Thus the laser operates
well within the required temperature range.~~

Obviously, the laser according to the invention
may be used for the same purposes as described in prior
5 art as mentioned above, and particularly to pump a
power laser composed of a fiber doped with erbium.